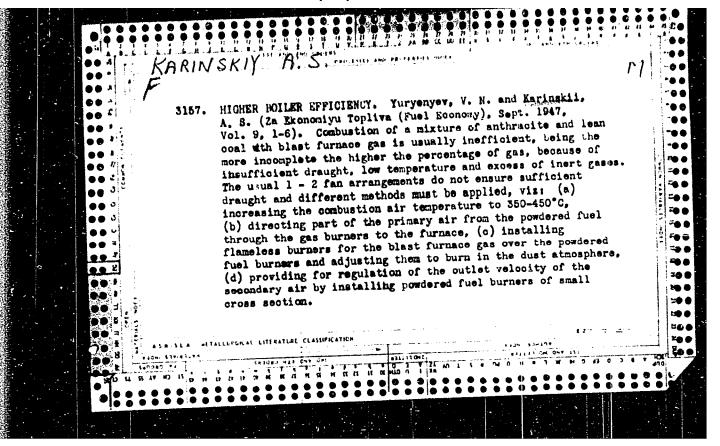
NIKITIN, A.A., kand. tekhn.nauk, dots.; KARINSKAYA, L.P., red.; SERGEYEVA, I.N., red.

[Machine tools for the machining of wheel pair axles; text-book on the subjects "Study of metals, technology of metals and special machines," "Study of metals, technology of metals and building materials" for the fifth and sixth year and graduating students specializing in "Car construction, operation and maintenance" and "Diesel locomotive operation, maintenance and repair"] Stanki dlia obrabotki osei kolesnykh par; uchebnoe posobie po distsiplinam "Metallovedenie, tekhnologiia metallov i spetsstanki," "Metallovedenie, tekhnologiia metallov i konstruktsionnykh materialov" dlia studentov V, VI kursov i diplommikov spetsial nostei: "Vagonostroenie i vagonnoe khoziaistvo" i "Teplovozy i teplovoznoe khoziaistvo." Moskva, Vses. zaochnyi in-t inzhenerov zheldor. transporta, 1963. 79 p. (MIRA 17:3)



KARINSKIY, A. S.

PA-23T28

USSR/Engineering

Sep 1947

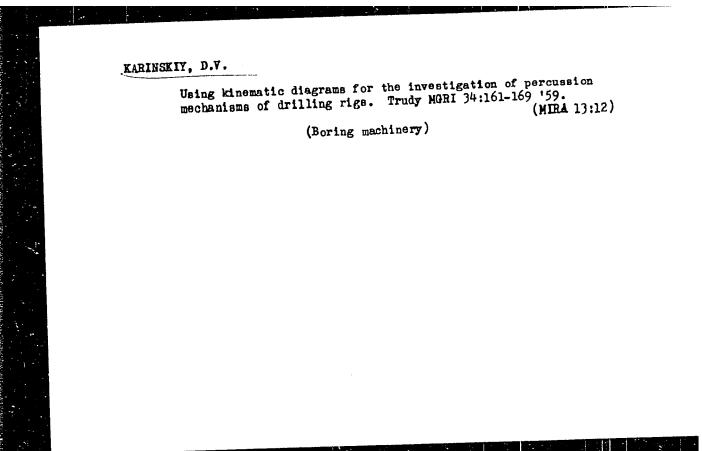
Boilers Fuel Conservation

"Increasing the Economy of Boilers Operating on a Compound of Coal Dust and Blast Furnace Gas. " V. N. Yurenev, A. S. Karinskiy, 52 pp

"Za Ekonomiyu Topliva" Vol IV, No 9

Deals with the use of this fuel compound in type KO-III-200 and IMZ-90/110 boilers. This method results in increased use of blast furnace gases. The use of coal dust is recommended because it is able to burn better without making any special adjustments of air supply. Certain special adaptions must be made, however, one of which is the heating of the air 3509 -450° C before it enters the combustion chamber. Illustrated with schematic diagrams, tables and graphs of operating data.

PA-23T28



AFANAS'YEV, Pavel Semenovich, kand. tekhn. nauk; BURKOV, V.I., inzh., retsenzent; ZARODZINSKIY, Z.K., inzh., red.; KARINSKIY, S.A., inzh., red.; LEYN, E.A., kand. tekhn. nauk, red.; NOVIKOV, D.Z., kand. tekhn. nauk, red.; OBRAZTSOV, S.A., inzh., red.; RUDNIK, M.S., kand. tekhn. nauk, red.; SAZONOV, A.G., inzh., red. izd-va; TIKHONOV, A.Ya., tekhn. red.

[Woodworking machinery]Derevoobrabatyvaiushchie mashiny; spravochmik. Moskva, Mashgiz, 1962. 575 p. (MIRA 15:12) (Woodworking machinery)

KARINSKIY, Sergey Sergeyevich; SAKHAROVA, I.M., red.; MAKAROVA, A.N., tekhn.red.; TARASOVA, N.M., tekhn.red.

[Rewarding the achievements of workers according to Soviet law]

Pooshchreniie za uspeshnyi trud po sovetskomu pravu. Moskva, Gos.

izd-vo iurid.lit-ry, 1961. 149 p. (MIRA 14:3)

(Labor laws and legislation) (Wages and labor productivity)

## KARINSKIY, S.Yu.

Limit equilibrium of a grainy medium near a round stamp. Trudy Sekt. mat. i mekh. AN Kazakh. SSR 2:128-137 '63. (MIRA 16:10)

KARINSHY, S.YU. (Alma-A+a)

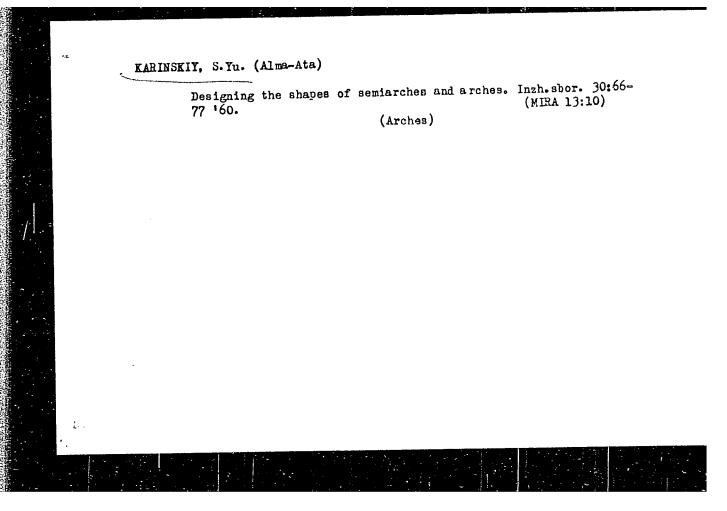
"On discontinuous of the problems of statics of loose media".

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow, 29 Jan - 5 Feb 64.

MOLYUKOV, I.D.; KARINSKIY, S.Yu.

Shapes of stable arches and seniarches. Inv.AN Kazakh.SSR.
Ser.mat. 1 mekh. no.7:95-101 '59. (MIRA 12:5)

(Arches)



APPROVED FOR RELEASE: 06/13/2000 CIA-RDP86-00513R000720720011-1"

KARINSKIY, S. YU.

The Solution of a Plane Problem in Connecting with the Statics of Loose Material. p. 178

TRANSACTIONS OF THE 2ND REPUBLICAN CONFERENCE ON MATHEMATICS AND MECHANICS (TRUDY VTOROY RESPUBLIKANSKOY KONFERENTSII PO MATEMATIKE I MEKHANIKE), 184 pages, published by the Publishing House of the AS KAZAKH SSR, ALMA-ATA, USSR, 1962

KARINSKIY, S.Yu. (Alma\_Ata)

Stable form of a loose medium near a rigid punch. Inzh. zhur. 3
no.2:300-311 163. (MIRA 16:6)

(Soil mechanics)

KARINSKIY, S.Yu. (Alma-Ata)

Discontinued solutions of the problem of the pressure of filling on supporting walls. Inzh.zhur. 5 no.2:316-323 165. (MIRA 18:4)

ACC NR AP6027513 SOURCE CODE: UR/0105/66/000/006/0038/0042

AUTHOR: Karinskiy, Yu. I. (Candidate of technical sciences)

ORG: Voronezh Polytechnical Institute (Voronezhskiy politekhnicheskiy institut)

TITLE: Optimal diode relay circuits of high reliability using unreliable relays

SOURCE: Elektrichestvo, no. 6, 1966, 38-42

TOPIC TAGS: optimal control, circuit reliability, mathematic analysis, circuit

ABSTRACT: The article deals with the general problem of improving the reliability of relay contacts through the method of circuit design using less reliable elements. An estimate of reliable relay-contact circuits of the hammock configuration is made. Operating with the definition that an optimal, reliable circuit is one which satisfies the quorum function (the best Boolean function for reliability improvement), the principle and methods of realization of such circuits are analyzed. Reliable iteration circuits are discussed and a comparative evaluation is made of various reliable diode relay circuit designs. The present mathematical circuit analysis is an approximate one, since it makes no allowance for the following factors: relay aging and winding and contact failures; decreased probability of relay operation with increased number of relays in the circuit; decreased relay reliability with increased number of relay contacts; and possible unreliability of the diodes and other circuit components. The

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UDC: 519.21:517.11

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#### CIA-RDP86-00513R000720720011-1

SOURCE CODE: UR/0413/66/000/019/0051/0051 (A, N) ACC NR. AP6035703 INVENTORS: Karinskiy, Yu. I.; Mikhaylov, V. V. ORG: none TITLE: A pulse relay for power direction. Class 21, No. 186555 SOURCE: Izobreteniya, promyshlennyye obraztsy, tovarnyye znaki, no. 19, 1966, 51 TOPIC TAGS: electric power engineering, power monitor, power supply, electric relay ABSTRACT: This Author Certificate presents a pulse relay for power direction. The relay operates on the principle of comparing the signs of the instantaneous values of the two quantities (current and voltage) at fixed instants of time. The relay includes a pulse shaper, a coincidence circuit, and an output device (see Fig. 1). simplify the relay, the coincidence circuit and the output device are made with Fig. 1.  $T_r$  - pulse transformer; UV1 and UV2 - controlled rectifiers of the coincidence circuit and of the output device;  $S_{t}$  - stabilitron tube UV2 621.316.925.2 621.318.56.016.2 UDC: Card 1.

controlled diodes. The coincidence circuit-controlled diode is fed a stabilized voltage from the protected object. This diode of the coincidence circuit is controlled by stabilized voltage pulses through a pulse transformer with a phase which is a function of the current phase of the protected object. Orig. art. has:									
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DROZDOV, A.D., dotsent, kand.tekhn.nauk; KARINSKIY, Yu.I., inzh.

Circuit for increasing the secondary-current multiplicity of magnetic transformer relays. Izv. vys. ucheb. zav.; elektromekh. no.1:96-98 '58. (MIRA 11:6)

1. Novocherkasskiy politekhnicheskiy institit. (Electric relays)

ACC NR: AP6026345

SOURCE CODE: UR/0144/66/000/007/0781/0788

AUTHOR: Karinskiy, Yu. I. (Candidate of Technical Sciences; Acting Docent)

ONG: Automation and Telemechanics Department, Voronezh Polytechnic Institute (Kafedra avtomatiki i telemekhaniki Voronezhskogo politekhnicheskogo instituta)

TITLE: Multipurpose contactless relay for maximum and minimum alternating voltage or current

SOURCE: IVUZ. Elektromekhanika, no. 7, 1966, 781-788

TOPIC TAGS: electric relay, system reliability, electric protective equipment, semiconductor device

ABSTRACT: A contactless relay for maximum or minimum alternating voltage or current which is relatively free of the shortcomings encountered in electromagnetic type voltage and current relays is discussed. It can be used in applications where demands are higher than those usually applied. The units and elements contained in the relay are described, as are operating principles, characteristics, and results obtained from a test model. The relay was found suited for use as a protective device and in automated systems contained in electrical systems, industrial installations, and transportation media. Tests revealed satisfactory electrical characteristics, temperature stability, and vibration resistance. The use of controlled

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VDC: 621.316.925+621.3.022

ACC NR. AP6026345

gates, tunnel diodes, silicon regulators, and other types of semiconductor devices and instruments for relay protection and automation makes it possible to obtain characteristics unobtainable in other designs. Orig. art. has: 23 formulas, 4 figures and 1 table.

SUB CODE: 09/SUBM DATE: 29 May 65/ORIG REF: 003

AUTHORS:

Drozdov, A.D., Doctor of Technical Sciences, Docent and

Karinskiy, Yu.I., Assistant

TITLE:

Longitudinal Differential Protection of Transformer-Line

Units with Electro-Magnetic Relays and Saturating

Transformers ( Prodol'naya differentsial'naya zashchita blokov liniya-transformator s elektromagnitnymi rele i

nasyshchayushchimisya transformatorami)

PERIODICAL: Izvestiya Vysshikh Uchebnykh Zavedeniy, Elektromekhanika, 1958, Nr 10, pp 94-103 (USSR)

ABSTRACT:

Lines connected direct to transformers and also short transmission lines employ longitudinal differential protection with pilot wires. Induction and polarised relays with mechanical retardation are being used for such schemes. The retardation compensates for the action of out-of-balance currents due to resistance of the pilot wires. These out-of-balance currents may be balanced by additional currents flowing in special balancing resistors. Then ideally there is no current in the relay on the occurrence of an external fault except the out-of-balance current resulting from

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differences between the current transformers and

Longitudinal Differential Protection of Transformer-Line Units with Electro-magnetic Relays and Saturating Transformers

differences between the resistances in the arms of the protective circuit. Mechanical or magnetic retardation can be used to compensate for these currents. This article describes a longitudinal differentially protected system with electro-magnetic relay type ET-520 and with magnetic retardation obtained by means of saturating transformers. When external faults occur the cores of these transformers are magnetised in such a way that the operating current of the protective system is increased. A schematic diagram of the protective circuit is given in Fig 1, it requires two pilot wires of length of up to 20 km with resistance up to 1500 ohms and capacitance up to 1.2 µF between conductors. The minimum operating current on the occurrence of an internal three-phase short circuit is 7.5 A with supply from one side and for two-phase faults it is 2.7 A. With supply from both sides the operating current is about halved. The operating current value can be adjusted by means of tappings on the primary windings of the saturating

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Longitudinal Differential Protection of Transformer-Line Units with Electro-Magnetic Relays and Saturating Transformers

transformer. The component parts of the circuit are described. Current filters convert the three-phase system of currents to single-phase. The saturating transformer in the protective circuit serves to set up retardation to prevent the protection from operating on magnetising current surges and to limit the voltage on the pilot wires. The characteristics of the saturating transformer are given in Fig 1. The design of saturating transformers is briefly discussed. The relay transformer serves to apply to the relay the difference between the line and balancing currents and to isolate the relay from the remaining protective circuits. The relay transformers have very low power losses. The characteristics of the relay transformer are given in Fig 1. The design of the protective circuit is then considered. The balancing circuit constants are first calculated so as to ensure that there is no relay current on the occurrence of an external fault. The design is based on the equivalent circuit for currents in the protective system given in

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Longitudinal Differential Protection of Transformer-Line Units with Electro-Magnetic Relays and Saturating Transformers

The circuit is balanced if the impedances of the balancing circuit and the linear circuit ABCD (Fig 2) have identical active and reactive components respectively. It is then shown how to calculate the various impedances and the capacitance connected across the relay. When the system is supplied from both sides the equivalent circuit for currents in the protective system becomes as shown in Fig 3. Calculations are then made of the currents and voltages in this circuit. The characteristics of the protective system were then studied. The balancing impedances and capacitors were selected to suit a pilot wire impedance of 1000 ohms with capacitance between pilot wires of 2 x 0.4  $\mu$ F. The retardation characteristics of the protection for the case when the impedance of the pilot wires corresponds to the tuning of the protection and the capacitance is  $2 \times 0.5 \mu F$ , are given in Fig 4. The retardation characteristics given in Fig 5 correspond to minimum resistance of the pilot wires (600 ohms) and low capacitance between them

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Iongitudinal Differential Protection of Transformer-Line Units with Electro-Magnetic Relays and Saturating Transformers

Tests of the protective system showed  $(3 \times 0.4 \mu F)$ . that the retardation characteristics vary a little over a wide range of resistance of pilot wires and capacitance between them. Reducing the capacitance between the pilot wires somewhat improves the retardation characteristics but impairs the sensitivity somewhat. The angular characteristic is defined as the relationship between the operating current of the protective system at one end of the block (for a certain value of current at the other end) and the phase angle between these currents. The angular characteristic given in Fig 6 is obtained with a secondary current at one end of 15 A flowing in phases B and C. It may be shown from the angular characteristic that the protection is more sensitive when the larger of the two currents is lagging. The angle of retardation of the protection can be adjusted by changing the induction in the saturating transformers, increase of the operating induction increases the angle of retardation. The operating time of the protective system was determined as function of the primary current.

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Longitudinal Differential Protection of Transformer-Line Units with Electro-Magnetic Relays and Saturating Transformers

In the independent part of the characteristic the operating time of the protective system was 35 m sec. The total operating time allowing for the output intermediate relay type EP-133 is 70 to 80 msec. Oscillograms of the voltage on the secondary winding of the insulating transformer when the pilot wires are cut are given in Fig 7. It will be seen that the capacitance between the pilot wires considerably reduces the voltage peak. With the pilot wires in good condition the mean value of voltage measured by a rectifier type voltmeter does not exceed 100 V. Breakage of the pilot wires does not cause false interruption of the protective system. Short circuits from the pilot wires do not cause false operation either. The power consumption of the protective system is 10 VA with a symmetrical three-phase current of 5A. Operating currents obtained with different types of fault are

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Longitudinal Differential Protection of Transformer-Line Units with Electro-Magnetic Relays and Saturating Transformers

tabulated. There are 7 figures and 3 references, 2 of which are Soviet and 1 English.

ASSOCIATION: Kafedra Elektricheskikh Stantsiy, Setey i Sistem Novocherkasskogo Politekhnicheskogo Instituta (Chair of Power Stations, Novocherkassk Polytechnical Institute)

SUBMITTED: 11th November 1958

Card 7/7

CG 1 15651-65 ENT(1)/ENA(h) Ped JR/0144/64/000/01?/1475/1482 ACCESSION NR: AY5013167 AUTHOR: Karinskiy, Yo. I.; Mikhaylov, V. V. TITLE: Contactless response element for transformer relays SOURCE: IVUZ. Elektromekhanika, no. 12, 1964, 4475-1482 MOPIC TAUS: electric transformer, electric relay, electronic vectifier Abstract: The article deals with the supplication problems in certain types of controlled rectifier devices used in conjunction with transformer relays. The voit-ampers and the response characteristics are discussed and the design parameters are determined on this basis. Specifically, two models of such relays with contactless response elements are described: DZT-1 with time delay and RHT-562 which is a current-unbalance relay; both are used for transformer protection and have so for proved successful in operation. They are considered supportor to electromagnatio type elements with regard to size, power consumption, like, resistance to shock and vibration. Orig. art. has 7 figures. ASSOCIATION: Hone BUB CODS: EO, EB ENGL: 00 SUBJUTUED: 15Ju164 JPR6 OTHER: 002 no her boy: Cord 1/1774

DROZDOV, A.D., doktor tekhn.nauk, prof.; KARINSKIY, Yu.I., inzh.

Longitudinal differential current protection of lines analogous to connecting wires. Izv. vys. ucheb. zav.; energ. 4 no.7:1-9 Jl '61. (MIRA 14:7)

1. Novocherkasskiy politekhnicheskiy institut imeni S. Ordzhonikidze. Predstavlena kafedroy elektricheskikh stantsiy, setey i sistem.

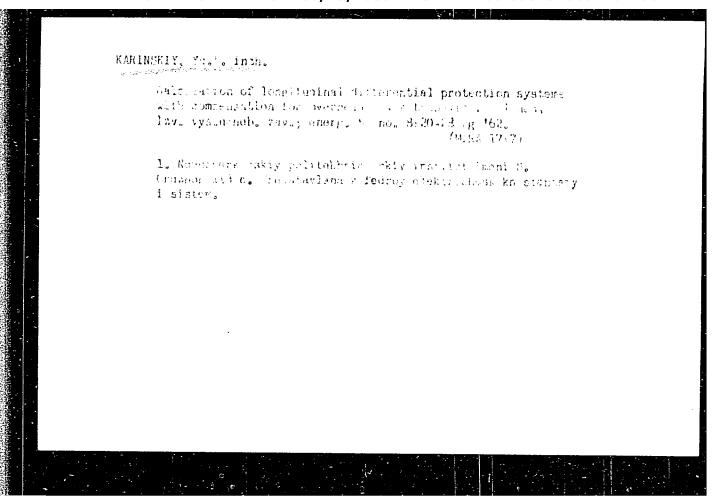
(Electric protection) (Electric power distribution)

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KARINSKIY, Yu.I., inzh.

Device for checkin the sonnecting wires of longitudinal differential protection systems of power transmission lines. Izv.vys.ucheb.zav.; energ. 7 no. 4:95-99 Ap '64. (MIRA 17:5)

1. Novocherkasskiy politekhnicheskiy institut imeni S.Ordzhonikidze. Predstavlena kafedroy elektricheskikh stantsiy, setey i sistem.



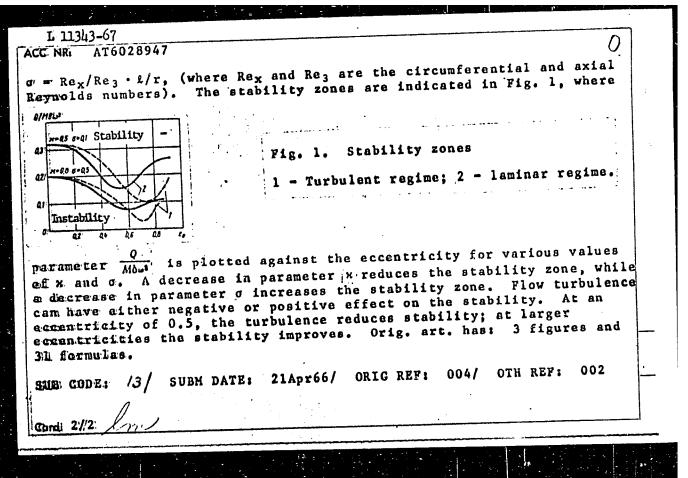
KARINSKIY, Yuriy Igorevich, kand.tekhn.nauk, starshiy prepodavatel';
MIKHAYLOV, Vladimir Vladimirovich, kand.tekhn.nauk, dotsent

Contactless sensitive device for transformer relays. Izv.vys.ucheb.
zav.; elektromekh. 7 no.12:1475-1482 '64.

(MIRA 18:2)

1. Kafedra elektricheskikh stantsiy, setey i sistem Novoch rkasskogo politekhnicheskogo instituta.

MI/DJ/GD code: UR/0000/66/000/000/0358/0378 L 11343-67 ENT(1)/EWT(m) AUTHOR: Karintsey, I. B. (Engineer) ORG: none TITLE: Rotation stability of centrifugal pump impellers SOURCE: Dinamika mashin (Dynamics of machinery); sbornik statey. McScow, Izd-vo Mashinostroyeniye, 1966, 368-378 TOPIC TAGS: fluid pump, centrifugal pump, centrifugal pump impeller, impelier stability, BEARING STABILITY ABSTRACT: An analysis is presented of the vibration stability of a rigid centrifugal pump limpeller mounted on short hydraulic bearings. Since the flow structure in this type of bearing is similar to that occurring in sliding bearings, the hydrodynamic equations previously derived for short sliding bearings were used in the analysis. A stability criterion was established as a function of four dimensionless  $\frac{Q}{A10\omega^3}$ , x, q and  $\epsilon_0$ . Here,  $Q = P_0(1 - k) \chi L$ ;  $P_0$  is the difparameters: ference between the inlet and exit pressures; 'x, ratio between inlet and total hydraulic resistance in the bearing clearance; M, shaft mass; r and & are the bearing radius and length, respectively; 6, radial clearance parameter;  $\epsilon_0$ , eccentricity;  $\omega$ , angular velocity; and Card 1/2



20167

S/114/61/000/004/002/006 E194/E435

26.2141

Martsinkovskiy, V.A., Engineer and

Karintsev, I.B., Engineer

TITLE:

AUTHORS:

The Influence of Radial Clearance Glands on the

Critical Speed of Feed Pump Rotors

PERIODICAL: Energomashinostroyeniye, 1961, No.4, pp.12-14

TEXT: Feed pump rotors are a complicated oscillatory system for which it is very difficult to provide an accurate theoretical calculation. The only existing method, proposed by Professor A.A.Lomakin (Ref.1) is approximate and a considerable series of experiments were made to assess its accuracy. An experimental feed pump rig was used to test a full-scale rotor of a feed-pump type \$\Pi \Pi \Pi 20-200\$ (PE 320-200) with two glands which were located either near the middle or adjacent to the bearings. The geometry and type of glands are given in tables 1 and 2. Tests were made with various values of pressure drop across the glands ranging from 0 to 60 atm. The influence of the diameter of single gap and multi-gap glands was investigated on a special single-disc rotor. The first critical speed in air was 2900 r.p.m. for the Card 1/9

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The Influence of Radial ...

single disc and 2340 r.p.m. for the full-scale rotor. Rotor vibration was made in the speed range of 0 to 8500 r.p.m. measured by inductive pick-ups recording on an electromagnetic oscillograph. Particular attention was paid to single-gap glands as experience with the feed pumps at the Cherepet power station has shown that they are most reliable in ensuring vibration stability of the rotor. A study was made of the influence on the value of the first critical speed, on the resonance amplitudes and on the unstable conditions of the rotor of the following parameters of single gap glands: the pressure drop on the glands, the radial gap, the length of the gap, the diameter of the gland, the eccentricity of the rotor relative to the gland, the place of location of the gland and the shape of In both these curves the critical the inlet edges of the gland. speed in r.p.m. is plotted on the y axis, in curve la as a function of pressure drop and in curve lb as function of the gap length. No influence of the shape of the inlet edges on oscillation of the rotor was found but this shape has a considerable influence on wear of the gland rings which were subject to erosion to a depth of about 1.5 mm after about an hour's working as shown in Fig. 2. Card 2/9

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The Influence of Radial ...

In this figure the place of wear is marked in black. The glands reduce the amplitude of resonance vibrations, particularly when the gap is reduced and the diameter and length of the gland is Unstable conditions, which are most dangerous, also occur with glands but the zones of instability for rotors with glands are much higher than for rotors in air. In the tests instability commenced at speeds of 7000 to 8000 r.p.m. with At higher pressure drops pressure drops not exceeding 10 atm. Results have also been obtained on they disappeared completely. the influence of the critical speed of rotors of the dimensions of individual gaps in 2 and 3 gap glands. The variants of gland tested are given in table 2; the construction and notation used In multi-gap glands clearances have will be seen from Fig. 3. In Fig.3 if the gap different influences in different designs. b2 is reduced the critical speed is reduced, the resonance amplitude is increased and instability becomes worse. clearances b<sub>1</sub> and b<sub>2</sub> have the opposite effect. experimental investigations show that glands increase the critical speed of the rotor. The dotted lines in Fig.l correspond to Card 3/9

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The Influence of Radial ...

critical speeds calculated by the method of Professor A.A.Lomakin for radial gaps in glands of 0.3 mm. In this particular case agreement with experiment is good. In Fig.lb which shows the influence of the gland length on the critical speed for various pressure drops, it will be seen that there is first a marked increase in the critical speed with the length of gland, but later This is in general agreement with the theoretical this tails off. The amplitude of resonance oscillations is much reduced curves. by the presence of a gland so that transition of the rotor through a resonance is not dangerous. Often the amplitudes are so small that the resonance speeds could not be accurately determined from There must be considerable damping forces both the oscillograms. It is most important to in the glands and in the plain bearings. Multi-gap glands differ in principle from determine these forces. single-gap in that they may reduce the critical speed of the rotor as compared with its value in air. Two-gap glands have no The use of a greater number of gaps advantages over single-gap. may be advantageous provided that the even-number clearances are large but the use of such glands will increase frictional losses Card 4/9

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The Influence of Radial ...

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and the optimum number should be selected on the basis of vibration stability, reduction in volumetric losses and disc The tests show that unstable conditions are dangerous friction. It is known that the cause of loss in high pressure feed pumps. of stability is friction between the rotor and the medium in the glands which sets up forces perpendicular to the line of centres. In multi-gap glands if the clearance b2 is small, then two and three gap glands can become sources of excitation of vibrations which commence at sub-critical speeds and are maintained over a Increasing the clearance b2 avoids these wide range of speed. It is also concluded that there is no point in oscillations. increasing the gland length above 60 mm in order to increase the critical speed of the rotor. The greatest effect in increasing the rigidity is obtained with glands near the centre of the rotor and these should, therefore, be used to increase the critical speed. The question of the influences of gland clearances on the critical speed is still open and for clearances of 0.25 to 0.3 mm, which are commonly used, the calculated critical speed of the rotor with a single pair of glands is in satisfactory agreement Card 5/9

S/114/61/000/004/002/006  The Influence of Radial  S/114/61/000/004/002/006  E194/E435  With experiment. There are 4 figures, 3 tables and 5 Soviet references.  Table 1.  1 - diagram of gland arrangement 2 - reference number 3 - length of the gland mm 4 - radial gap b mm 5 - notation of the points on the curves of Fig.la and b.  Kpnc. 1 20 0.10 × 0.25 0 0.40	_		20167
Table 1.  1 - diagram of gland		The Influence of Radial	S/114/61/000/004/002/006 E194/E435
Table 1.       Схема расположения уплотнения зазор b. мм       Плина зазор b. мм       Обозначение точек         1 - diagram of gland arrangement       2 - reference number       1 20 0.10 × 0.25 0.25       0 0.25 0.25       0 0.25 0.25       0 0.40 0.25       0 0.40 0.25       0 0.40 0.25       0 0.40 0.25       0 0.40 0.40 0.40       0 0.75 0.40 0.40		<del>-</del>	4 figures, 3 tables and 5 Soviet
arrangement  2 - reference number  3 - length of the gland  mm  4 - radial gap b  mm  5 - notation of the points  on the curves of  Fig.la and b.			Плина Радиальный Обозначение
		arrangement  2 - reference number  3 - length of the gland mm  4 - radial gap b mm  5 - notation of the points on the curves of	1   1   1   1   20   0,10   ×   0,25   0   0,25   0   0,25   0   0,25   0   0,25   0   0,25   0   0,25

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The Influence of Radial ...

#### Table 2.

- 1 gland arrangement
  2 notation of the points on the curves of Fig.4a and b.

Тип уплотнений	Na n/n	, imi, NN	la=la MM	ь. ии	b <sub>1</sub>	b <sub>a</sub>	b.		зидче Точек
0, 0, 0, 0	1 2 3 4 5 6 7	20 20 20 20 20 20 20 20	15 15 15 15 15 15 15	0,20 0,20 0,20 0,20	0,25 0,25 0,25 0,25 0,20 0,20	0,45 0,75 1,00 0,20 0,40	0,20 0,20 0,20 	О Д	K pnc. 4.6 K pnc 4. a

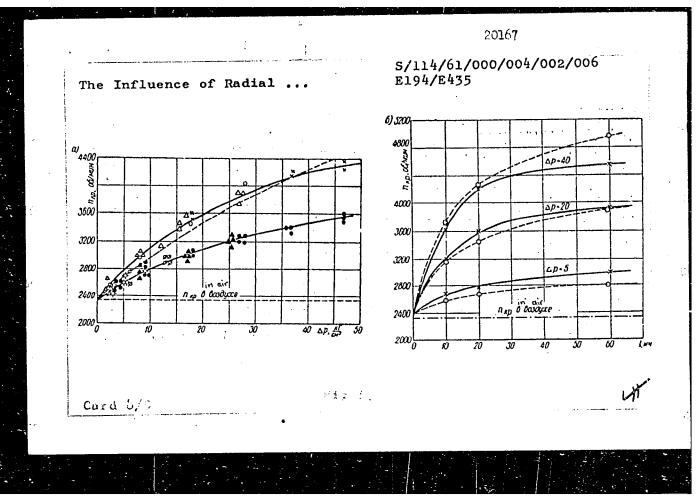
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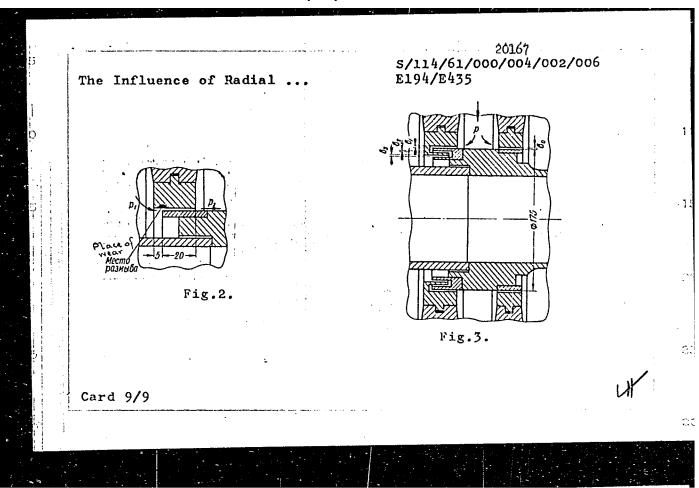
Card 7/9

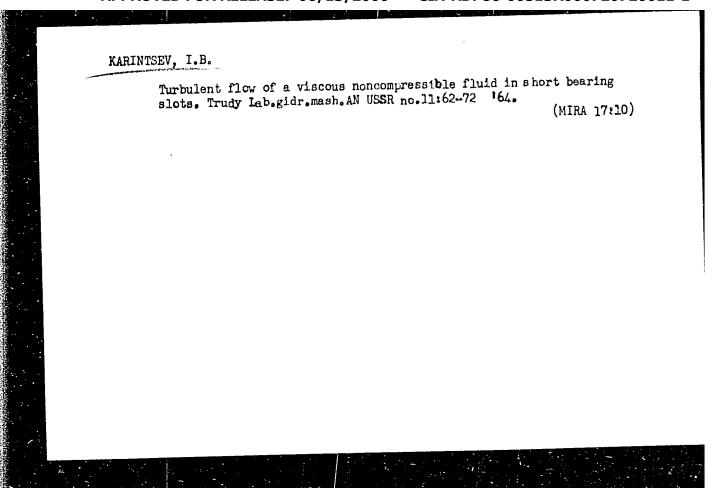
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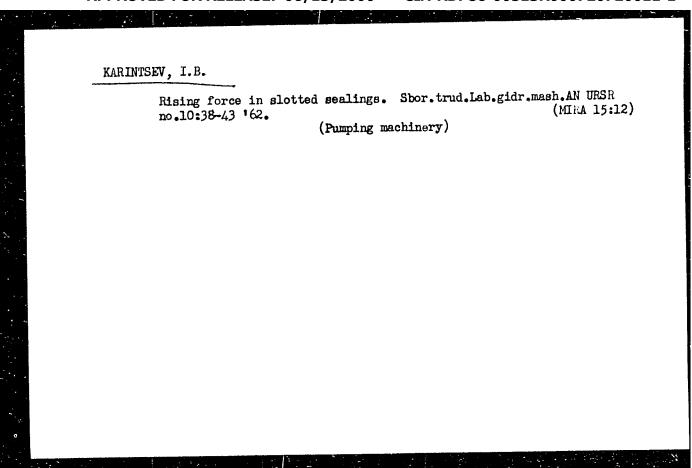
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### KARINTSEV, I.B.

Stability of the motion of rotors of hydraulic machines on short supports of liquid friction. Dop. AN URSR no.3:327-331 '64.

1. Laboratoriya gidravlicheskikh mashin AN UkrSSR. Predstavleno akademikom AN UkrSSR G.I. Sukhomelom [Sukhomel, H.I.].

CHUSOV, V.G., kandidat tekhnicheskikh nauk; KARINTSEVA, I.N., redaktor; TARASENKO, Z.K., tekhnicheskiy redaktor

[Distillery equipment] Oborudovanie spirtovykh zavodov. Moskva, Pishchepromizdat, 1950. 330 p. (MLRA 7:8) (Distillation apparatus)

KARINISKIY, V. A.

Kerintskiv. V. A. and Zatsepina-dizertinskaya, T. S. "The phenomenon of intensive movement of the mercury bulb during microanalystic reaction of exposed mercury," Sbornik nauch trudov (Rost. n/D gos. med. in-t), Vol. VIII, 1948, p. 55-57

SO: U-2868, Letopis Zhurnal'nykh Statey, No. 1, 1949

VASIL'TSOV, V.D.; VOLODARSKIY, L.M.; VOLCHENKO, M.Ya.; GALETSKAYA, R.A.; IROV, N.I.; KARINYA, L.F.; KOHOVALOV, Ye.A.; MATVIYEVSKAYA, E.D.; PETRESKU, M.I.; RUDAKOV, Ye.V.; SAYFULINA, L.M.; SKVORTSOVA, A.M.; SOKOLOVA, N.M.; SOTNIKOVA, I.A.; STOLPOV, N.D.; SURKO, Yu.V.; TEM, V.A.; TRIGULENKO, M.Ye.; FIRSOVA, Yu.V.; SHABUNINA, V.I.; YUMIN, M.N.; RYABUSHKIN, T.V., doktor ekon. nauk, otv. red.; ALAMPIYEV, P.M., red.; PAK, G.V., red.; GERASIMOVA, D., tekhn.red.

[Ecoromy of socialist countries, 1960-1962] Ekonomika stran sotsializma, 1960-1962gg. Moskva, Izd-vo "Ekonomika," 1964. 261 p. (MIRA 16:12)

1. Akademiya nauk SSSR. Institut ekonomiki mirovoy sotsialisticheskoy sistemy.

(Communist countries--Economic conditions)

Most important fire power. Voen. znan. 37 no.11:8-10 N '61.

(Artillery) (Rockets (Ordnance)) (World politics)

Countary : UDER M Caragery CULTIVATED PLANTS COMMERCIAL. Diefferous. Sugar-Ass. Jour. : REF ZHUR-BIOL..21,1952,NO-96063 Author : Mush. M.F.; Karionova. A.S. ... : All - mion Tett. Tar. Inst. of Oil and Pesential Oil-\* 2.34.300 i Taitai : Proplenting doil Treatment for Sunflowers Orig. Pde. : Y ab.: Eratkiy otohet o nauchno-isoledov. rabote Vses. n.-1. in-to Physhichm. 1 efiromaslichm. kul!tur za 1956 g., Mrasnoder, "Sow Kubad", 1957, 225-227 : Pielo tifals on the "eydelevakiy Experimental will (Belgorodskaye Obloat) here shown that the dostinada. application of cultivation at the moment weeds app ar in mass sharply reduces the weed choking in samplower plantings. Proplanting treatment considerably augments the yield (by 2.5-4.2 out/ha). --A.S. Bearing Crops Carl: 1/1

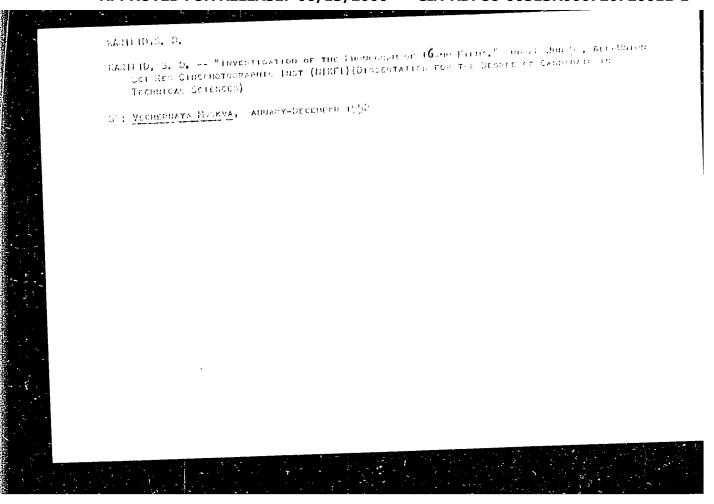
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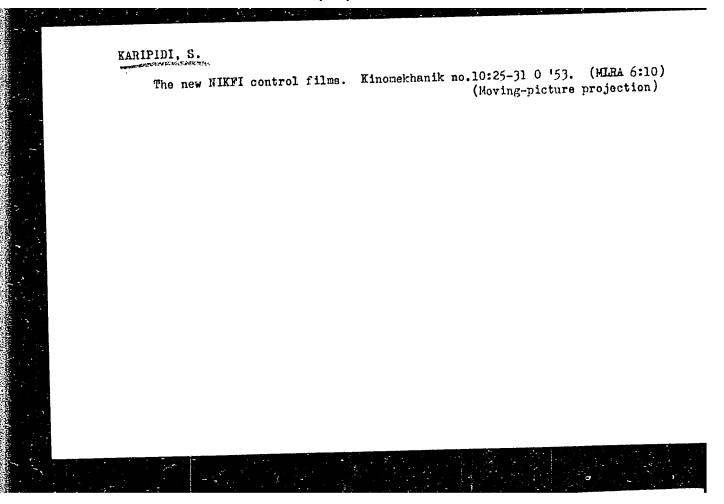
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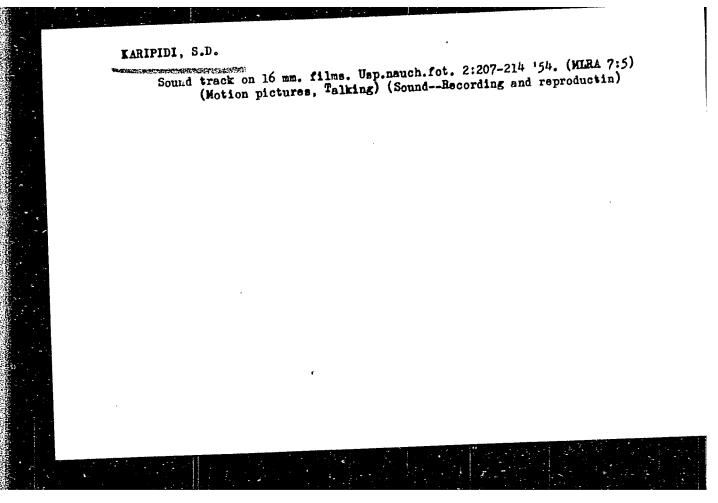
KARIOZEN, Zofia

Changes in the electrophoretic composition of blood serum proteins in the cases of acute posoning with chemical substances. Med. pracy 16 no.4:293-299 165.

1. Z Dzialu Klinicznego Instytutu Medycyny Pracy w Lodzi (Dyrektor: doc. dr. med. J. Nofer).





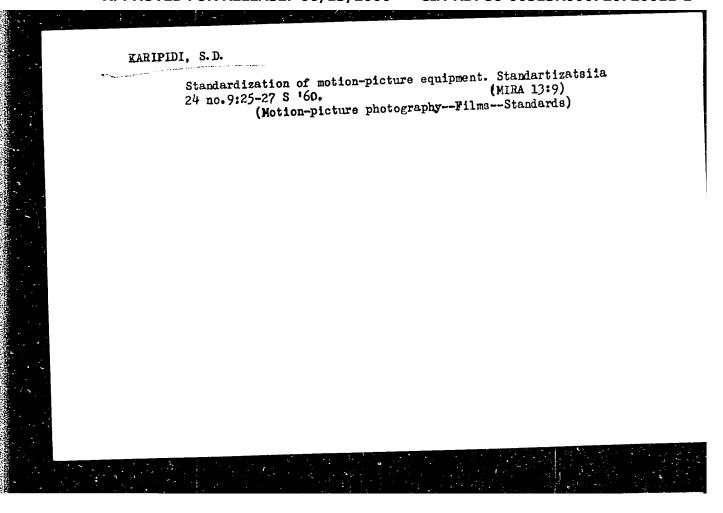


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KARIPIDE Sekrat Dmitrivavich; YAKOBSON, A.Th., redaktor; CHICHERIN, A.N., tekmicheskiy redaktor

[Gontrol films] Kontrol'nye fil'my. Moskva, Gos. izd-vo "Iskusstva," 1956. 91 p. (Mira 10:1)

(Motion picture projection)



NOVIK, F.S.; KARIPIDI, S.D.

Lenses for harrow-film motion-picture cameras. Standartizatsiia (MIRA 14:11)
25 no.11:43-44 N '61.

(Motion-picture cameras—Equipment and supplies)

PROVORNOV, Sergey Mikhaylovich; GOLOD, Iosif Semenovich; EERSHTEYN,
Naum Davydovich. Prinimal uchastiye KARIPIDI, S.D., kand.
tekhn. nauk, starshiy nauchnyy sotr.; EYSYNONT, L., red.;
PEREGUDOVA, M., tekhn. red.

[Equipment for motion-picture film printing]Kino-kopiroval'-

[Equipment for motion-picture film printing kino-kopitoval naia apparatura. Moskva, Iskusstvo, 1962. 314 p. (MTRA 15:10)

(Motion-picture photography--Equipment and supplies)

KARIPIDI, Sokrat Dmitriyevich; BOGATOVA, V.S., red.

[Control of the quality of motion-picture projection] Kontrol' kachestva kinopokaza. Izd.2., ispr. i dop. Moskva, Iskusstvo, 1964. 170 p. (MIRA 18:3)

0

USSR / Plant Diseases. Diseases of Cultivated Plants.

: Ref Zhur - Biologiya, No 22, 1958, No. 100587 Abs Jour

Author

: Karis, H.

Inst

: Estonian AS

Title

: The Incluence of Some Micronutrients on the Resistance of Tomatoes to Macrosporium and Phytophthora Infections

Orig Pub

: Eesti Pollumaj. Akad. teaduslike tööde kogumik, Sb. nauchn. tr. Est. s.-kh. akad., 1957, 3, 127-133

Abstract

: Solutions of the salts of KMnO4 - 0.05%, CuSO4 and H3B03 - 0.01 and 0.026, (NH4) MoO4 - 0.026 were used for the pre-sowing treatment of the seeds and the apraying of tomato plants during the formation of the fruits. Control seeds were soaked in distilled water. Mn and Cu appreciably delayed and lowered the infection of the plants by macrosporium and phytophthora. B also had a positive influence on the resistance to macrosporium.

Card 1/2

16

Card 2/2

BONCH-BRUYEVICH, A. M. VARGIN, V. V. IMAS, Ya. A. KARAPETYAN, G. O. KARIS, Ya. E. TOLSTOY, M. N. and FEOFILOV, P. P.

"Luminescence and induced radiation of a glass activated by neodymium."

The report gives the absorption and luminescence spectra of glass containing 0.1--10% neodymium. Stimulated emission in the region of 1.06 H, observed in specimens, was investigated at room and nitrogen temperatures.

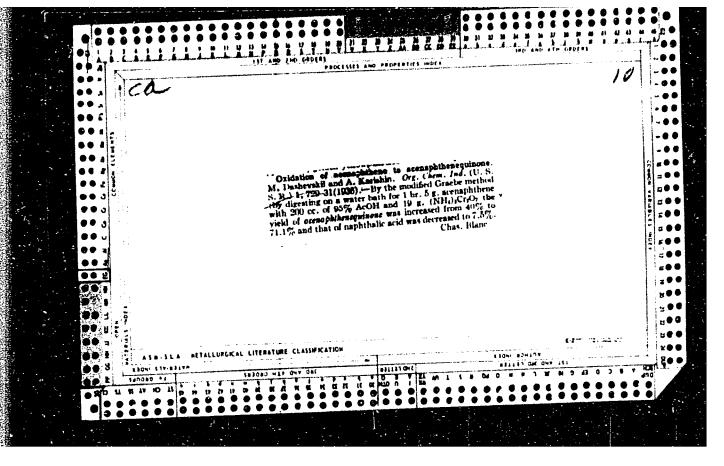
Report presented at the 11th conference on Luminescence (Molecular luminescence and luminescence analysis) Minsk, 10-15 Sep 1962

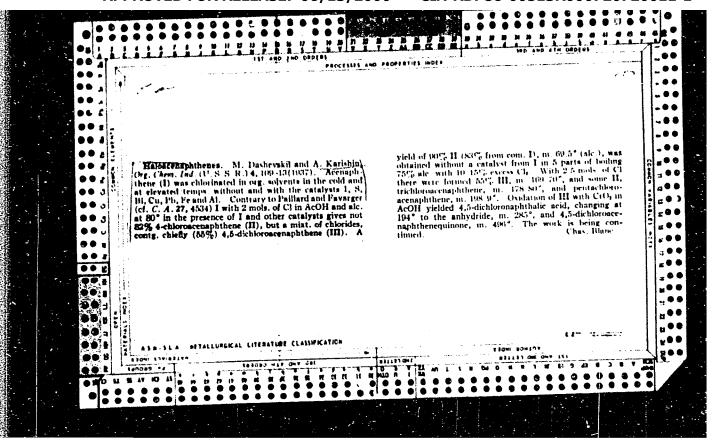
GOLOTA, Ya.A., kand.biolog. nauk; CHEPUROV, K.P., prof.; KARISHEVA, A.F., aspirant

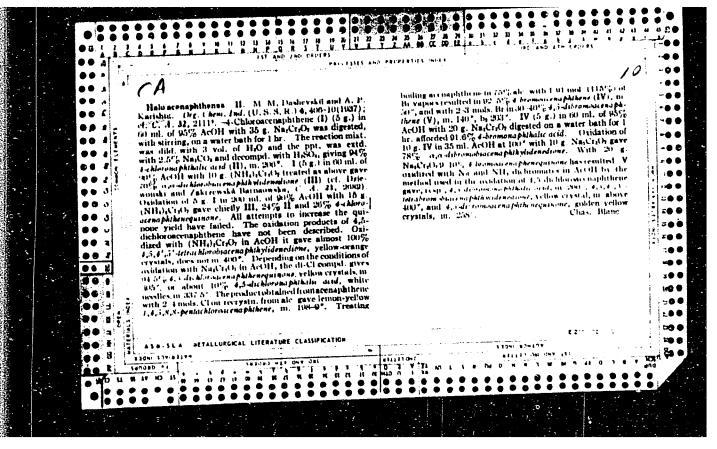
Methods for detecting living Leptospira in thoracic and yentral transudates of piglets. Veterinariia 40 no.5:29-30 My 163. (MIRA 17:1)

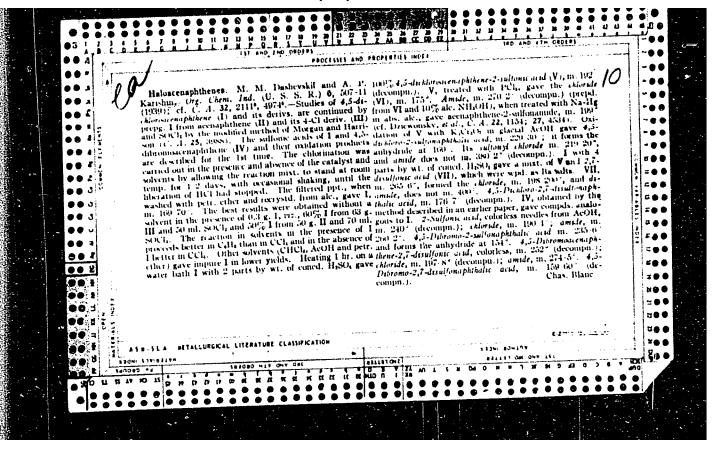
1. Ukrainskiy nauchno-issledovatel'skiy institut zemledeliya.

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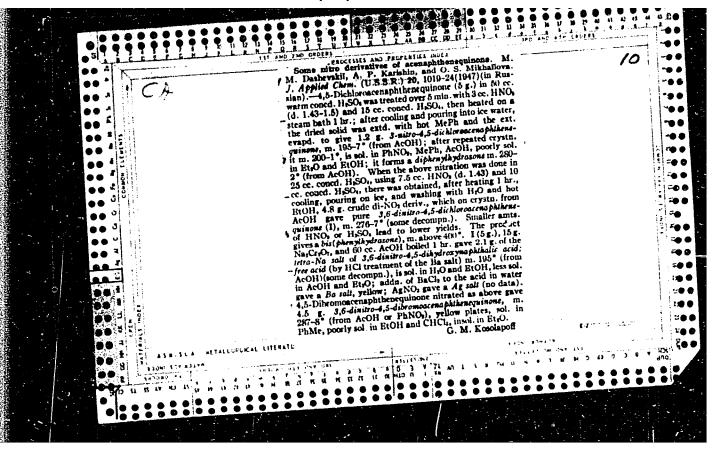








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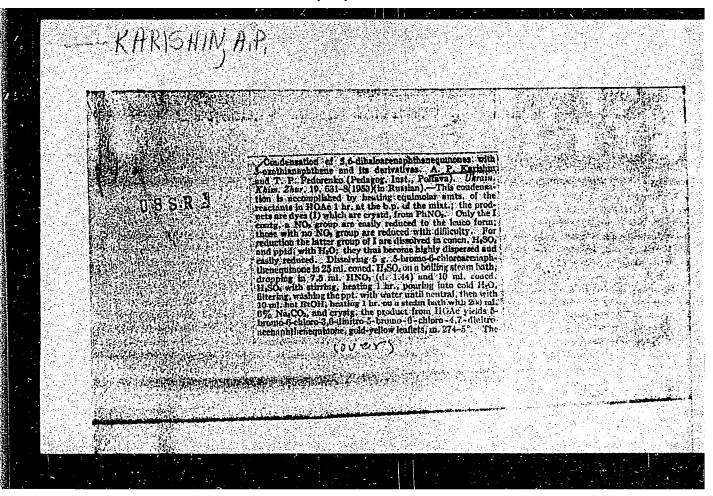
KARISHIN, A.P.

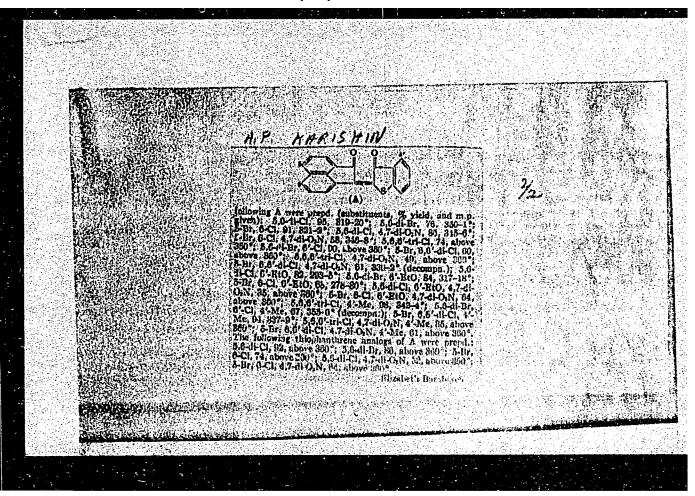
Halogen derivatives of arenaphthaneoutnous. A P. Katishin (Pedarog: Inst., Politava). Ukrais: Kaiss-Lau-16. nos-12.1952 (in: Russian). ct. Morgan and Harrison. (C.A.25, 3988.—Heating 5 g. 4.5-dichloroacenaphthene) with 20 g. NacCriO and 400.

5.6-slichloroacenaphthene) with 20 g. NasCr4O; and 400 ml. AcOll 1 hr. on a steam bath gave on enoling a solid product which was washed free of Cr with H<sub>2</sub>O. Extin. with hot AcOll 1 loft behind \$4'.5.5'-letrathlorobicfacensphilepidene). 111'-dione, orange, does not m below \$60° (from PhNO.); this is obtained in 20% yield if (NH<sub>2</sub>)-Cr<sub>2</sub>O; is used as the oxidant. The filtrate after evapn; was heated on a steam hath 1 hr. with stirring with 550 ml. PhBr and 200 ml. 6% Na<sub>2</sub>CO<sub>2</sub>; acidification of the aq. layer gave 0.7 g. 45-dichloronaphthatic anhydride, in 337-8° (from AcOH), which is obtained in 35% yield if the oxidation lasts 6 hrs. under the above conditions. The PhBr ext. heated on a steam bath 5 min; with 25-30 ml. 40% NailSO, gave a ppt. of the bisulfite adduct; which boiled with H<sub>2</sub>O 20 min; gave 54% 4.6-dichloroacenaphthenequinone, golden yellow, m. 803-5° (from AcOH). Refluxing this quinone (2 g.) with 1 2 g. 3-hydroxythianaphthene in AcOH 2 hrs. gave 95% 2-thionaphthene 8'-(4.5-dichloroacenaphtheisenedige (A), red., m.

519-26! (Irom PaCl or PhNO<sub>1</sub>). Heating 4,5-dichloromaphhalic subydride 3 hrs. with 25% NH<sub>4</sub>OH gave 65%
corresponding smide, m. 320-30' (Irom PhBr). Heating 5 g.
4,5-dihromoscensphthene in 60 ml. AcOH to 100', addn.
of 15 g. (NH<sub>4</sub>)Cr<sub>2</sub>O<sub>2</sub> over 8 mln. (vigorous reaction) results in
complete reaction within 15 mln; diln. with H<sub>4</sub>O and treatment with 6% Na<sub>2</sub>CO<sub>3</sub> with heating 1 hr, gave 16% insol.
4,4',5,5'-letrabromabiliacenaphhylidene) 1,1'-dione, brick
red, does not m. below 360' (Irom PhNO<sub>1</sub>). Similar oxidation over 10 mln. with Na<sub>2</sub>Cr<sub>2</sub>O<sub>3</sub> gave 18% 4,5-dibromoacenaphthenequisone, golden yellow, m. 238-0' (Irom AcOH
ov PhCl); meno-phenyhydrasone, m. 189-00' (Irom PhBr). Letting 5 g. 4-bromo-scaloroacenaphthene,
0.01 g. FeCl<sub>2</sub> and 2 ml. SO<sub>2</sub>Cl<sub>3</sub> stand 8 hrs. gave after treatment with Bt<sub>2</sub>O<sub>3</sub> 3,8 g. 4-bromo-5-chloroacenaphthene,
0.01 g. FeCl<sub>3</sub> and 2 ml. SO<sub>2</sub>Cl<sub>3</sub> stand 8 hrs. gave after treatment with Bt<sub>2</sub>O<sub>3</sub> 3,8 g. 4-bromo-5-chloroacenaphthene,
153-5' (Irom AcOH). This (5 g.) oxidized with 15 g.
(NH<sub>4</sub>)Cr<sub>2</sub>O<sub>3</sub> added at 100' to AcOH soln, over 8 mln, gave
21% 6.4'-dibremo-5-5'-dichlorobir(acenaphthydidene)-1,1'dional, brick red, does not m. below 300' (Irom PhNO<sub>3</sub>). Use
of 25 g. Na<sub>2</sub>Cr<sub>2</sub>O<sub>3</sub> in the solve oxidation, added at 100' at
once, gave 40% +bromo-5-chloroacenaphthenequinons; brown,
m. 307-9' (Irom PhBr or AcOH); hisulfile compound forms
crystalis on treatment of PhBr soln, with NaHSO<sub>4</sub>; monophenyhydrosone, m. 203-4' (from AcOH). The aq. layer
(Irom PhBr). Dihaloacenaphthenequinones and correspending maphthalic anhydrides form isomorphous mixts;
thus the two 4,5-dichloro derivs, crystallize together

1





KARISHIN, A.P.

USSR/Chemistry - Organic chemistry

Card 1/1

Pub. 116 - 18/30

Authors

Karishin, A. P., and Fedorenko, T. P.

Title

Condensation of dihaloidacenaphthenequinones with o-diamines. Part 1.

Periodical

Ukr. khim. zhur. 21/3, 373-376, June 1955

Abstract

Experiments were conducted to determine the condensation reaction of dihaloidacenaphthenequinones and dihaloiddinitroacenaphthenequinones with o-phenylenediamine, 2,3-toluylenediamine, 3,4-toluylenediamine, 5-bromo-2, 3-toluylenediamine and 1,2-naphthylenediamine. It is shown that the condensation reaction is perfectly easy in an acetic acid medium when the solution is heated to a boiling point. The properties of twenty-five new acenaphthylenequinoxalines are listed. Three USSR references (1947-1953). Table.

Institution:

State Pedagogical Institute, Poltava

Submitted

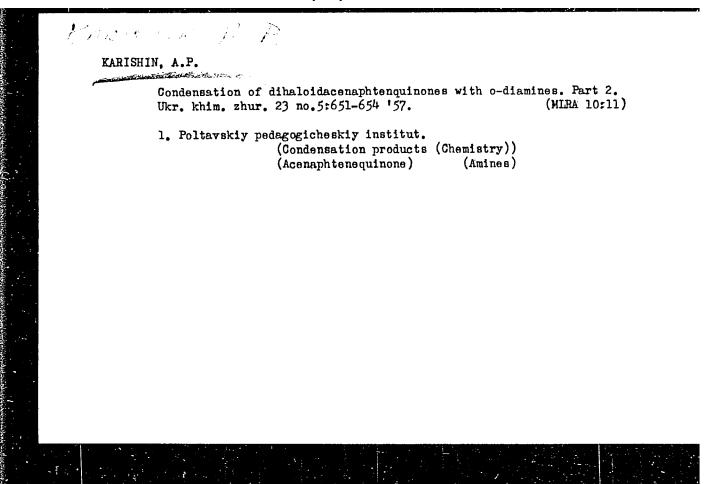
March 12, and September 13, 1954

# KARISHIN, A.P.; KUSTOL, D.M.

Condensation of haloacenaphthenequinones with inodoxyl. Ukr.khim. zhur. 22 no.2:229-231 '56. (MLRA 9:8)

1. Poltavskiy gosudarstvennyy pedagogicheskiy institut. (Indoxyl) (Acenaphthenequinone)

Cxidation of acenaphthene in sulfuric acid to naphthalic acid. Zhur.
prikl.khim.29 no.6:955 Je '56. (MIRA 9:9)
(Acenaphthene) (Naphthakic acid)



AUTHORS:

Karishin, A. P., Kustol, D. M.

79-28-3-29/61

TITLE:

On the Problem of the Synthesis of Naphthalimide and its Derivatives (K voprosu o sinteze naftal'imida i yego

proizvodnykh)

PERIODICAL:

Zhurnal Obshchey Khimii, 1958, Vol. 28, Nr 3, pp. 692-695

(USSR)

ABSTRACT:

According to the authors' opinion an incorrect conception prevails in publications on the conditions of the reaction of naphthalimide and its derivatives to the corresponding imides. It was found that the anhydride of naphthalic acid and its monohalide- and mononitroderivatives can be converted to the corresponding imides by means of 15-16 % ammonia solution at 60-90°C in the course of 30 minutes, the yield being 98 %. This reaction mainly proceeds passing through the ammonium salt of the monoamide of naphthalic acid according to the mentioned scheme. This ammonium salt is formed energetically already at 50-60°C, it is easily soluble in water but is very unstable, and almost completely converts to naphthalimide (97 %). When this salt solution

Card 1/3

On the Problem of the Synthesis of Naphthalimide and its 79-28 3-29/61 Derivatives

is acidified the monoamide of the naphthalic acid is precipitated as precipitate, which in boiling with water or in drying converts to naphthalanhydride (96 %) and to naphthalimide (4 %). The potassium salt of the monamide of naphthalic acid could be separated in free state. This proves the above mentioned opinion that in the ammonium salt solution of the monoamide of naphthalic acid the naphthalimide is formed as a side product in the reaction process. When naphthalic acid is used for the synthesis of naphthalimide its ammonium salt is formed in the reaction with aqueous ammonia, which converts to the naphthalimide only with a yield of 70 % in boiling the solution for six hours; this points to a preferred use of the anhydride and of a lower temperature. The anhydride of dihaloidnaphthalic acids convert more difficultly to the imides. There are 11 references, 6 of which are Soviet

Card 2/3

79-28 3-29/61 On the Problem of the Synthesis of Naphthalimide and its Derivatives

Poltavskiy gosudarstvennyy pedagogicheskiy institut Poltava State Pedagogic Institute) ASSOCIATION:

July 9, 1957 SUBMITTED:

Card 3/3

5(3)

SOV/79-29-6-34/72

AUTHORS:

Karishin, A. P., Kustol, D. M.

TITLE:

Synthesis of the 1,1'-Dinaphthyl-8,8'-dicarboxylic Acid From Naphthalimide (Sintez 1,1'-dinaftil-8,8'-dikarbonovoy kisloty

iz naftalimida)

PERIODICAL:

Zhurnal obshchey khimii, 1959, Vol 29, Nr 6,

pp 1928 - 1930 (USSR)

ABSTRACT:

In industry 1,1'-dinaphthyl-8,8'-dicarboxylic acid is frequently used for the synthesis of the anthanthrone dyes. It is known from publications (Ref 1) that 1-naphthyl amine-8-sulfo acid is used as initial product for their industrial synthesis. In order to transform this acid into the 1,1'-dinaphthyl-8,8'-dicarboxylic acid a series of complicated operations has to be performed. This acid may be obtained by a much simpler method from naphthalimide which is an easily accessible product (Ref 2). The method of the conversion of naphthalimide into the lactam of the 1-amino-8-naphthoic acid (naphthostyryl) with a yield of 56.5% as well as also the conversion of the latter into 1,1'-dinaphthyl-8,8'-dicarboxylic acid (38.5% yield) are described

Card 1/2

in publications (Ref 3). The authors elaborated the methods of

Synthesis of the 1,1'-Dinaphthyl-8,8'-dicarboxylic Acid SOV/79-29-6-34/72 From Naphthalimide

> converting naphthalimide into 1,1'-dinaphthyl-8,8'-dicarboxylic acid, viz without preceding separation of the lactam of 1-amino-8-naphthoic acid (72% yield). It was found that the lactam of the 1-amino-8-naphthoic acid may be obtained by the action of gaseous chlorine on the alkaline solution of naphthalimide at 15-17° with a yield of 86.2%. There are 4 references, 3 of which are Soviet.

ASSOCIATION: Poltavskiy gosudarstvennyy pedagogicheskiy institut (Poltava

State Pedagogical Institute)

SUBMITTED: February 3, 1958

Card 2/2

CIA-RDP86-00513R000720720011-1" APPROVED FOR RELEASE: 06/13/2000

5 (3)

AUTHORS:

Karishin, A. P., Kustol, D. M.

SOV/79-29-7-29/83

TITLE:

Condensation of the Halogen Naphthalic Acid Anhydrides With

Resorcin (Kondensatsiya galoidnaftalevykh angidridov s

rezortsinom)

PERIODICAL:

Zhurnal obshchey khimii, 1959, Vol 29, Nr 7, pp 2241 - 2243

(USSR)

ABSTRACT:

The halogen naphthalene fluoresceins (VIII) and (II) described in references 1 and 2 of which no melting points are given, and the bromine- and iodine derivatives of 5'-chloro- and 5'-bromonaphthalene fluoresceins, the constants of which are not given, may be obtained with optimum yields if the condensation with resorcin at 180-185° is carried out in the presence of anhydrous tin chloride within 30-40 min. Under these conditions the yield in halogen naphthalene fluoresceins is 70-74%, computed for the anhydride consumed in the reaction (35-40%). At higher temperatures up to 200-210° a higher amount of anhydrides enters the reaction. In this case, however, the yield in fluoresceins is reduced, since a large number of resins is formed. The formation of resins brings about a higher consumption of tin chloride. In the bromination and

Card 1/2

5(3) AUTHOR:

Karishin, A. P. Kustol, D. M.

SOV/79-29-8-67/81

TITLE:

On Some Nitro-and Amino Derivatives of 4,5-Dichloroacenaphthene

PERIODICAL:

Zhurnal obshchey khimii, 1959, Vol 29, Nr 8, pp 2745-2747 (USSR)

ABSTRACT:

The nitration of 4,5-dichloroacenaphthene (I) was investigated by G. T. Morgan and H. A. Harrison (Ref 1) who synthesized dichlorodinitroacenaphthene (melting point 200°) in the course of this process. They, however, did not detect the structure of this compound; indications as to the yield are also missing. The authors found that by the nitration of 4,5-dichloroacenaphthene (I) according to the instructions given by Morgan and Harrison dichlorodinitroacenaphthene (II) with a melting point of 251 - 252° and a yield of 45 - 50% is obtained. Further experiments made it possible to increase the yield of (II) up to 72%. The produced dichlorodinitroacenaphthene (II) was consequently transformed into dichlorodiaminoacenaphthene (III), tetrachloroacenaphthene (IV), and in tetrachloronaphthalic acid (V) in that order. By the oxidation of this acid (V) only 4,6-dichlorohemimellitic acid (VI) is obtained which has already been

Card 1/2

On Some Nitro- and Amino Derivatives of 4,5-Dichloroacenaphthene

SOV/79-29-8-67/81

described in publications (Refs 2, 3) (Scheme). Thus the structure of all recently synthesized compounds was determined. Furthermore, the imide of tetrachloronaphthalic acid was obtained. There are 3 references, 1 of which is Soviet.

ASSOCIATION: Poltavskiy gosudarstvennyy pedagogicheskiy institut

(Poltava State Pedagogical Institute)

SUBMITTED: July 7, 1958

Card 2/2

· --5(3) AUTHORS:

Karishin, A. P., Baklan, V. F.

507/79-29-9-52/76

TITLE:

N- Alkyl Derivatives of Naphthaliside and of Halogen Naphthalimides

PERIODICAL:

Zhurnal obshchey khimii, 1959, Vol 29, Nr 9, pp 3048-3050

(USSR)

ABSTRACT:

Some N-alkyl derivatives of naphthalimide are described in publications (Footnote). In order to investigate the properties of naphthalimide and its halogen derivatives they were alkylated. The alkylation was made by reacting potassium naphthalimide with the corresponding alkyl bromides in sealed ampoules at 150°. It was found that potassium naphthalimida, compared to the halogen derivatives, is more easily alkylated. Potassium naphthalimide necessary for the synthesis of the alkyl derivatives of naphthalimide was obtained in anhydrous as well as in aqueous-alkaline solution. In order to identify the preparations obtained they were alkylated and the alkyl derivatives were found to be identical. Several hitherto unknown compounds were synthesized. The N-alkyl derivatives of naphthalimide and of halogen naphthalimides are tabulated?

Card 1/2

They have the following structure:

CIA-RDP86-00513R000720720011-1" **APPROVED FOR RELEASE: 06/13/2000** 

507/79-29-9-52/76

N-Alkyl Derivatives of Naphthalimide and of Halogen Naphthalimides

 $[R = C_2H_5, C_3H_7, C_4H_9, C_5H_{11}, C_6H_{13}; X = H,Cl,Br].$ There are 1 table and 1 reference (Footnote).

ASSOCIATION: Poltavskiy gosudarstvennyy pedagogicheskiy institut (Poltava

State Pedagogical Institute)

SUBMITTED: July 21, 1958

Card 2/2

KARISHIN, A.P.; KUSTOL, D.M.

Synthesis of 4-halo derivatives of a lactam of 1-amino-8-naphthoic acid (4-halonaphthostyryles) based on acenaphthene. Zhur.ob.khim. 31 no.5:1655-1660 My '61. (MIRA 14:5)

1. Poltavskiy gosudarstvennyy pedagogicheskiy institut.
(Naphthoic acid)

KARISHIN, A.P.; KUSTOL, D.M.

Condensation of 5-fluoroacenaphthenequinone with 3-oxythionaphthene and its derivatives. Zhur.ob.khim. 32 no.10:3142-3143 0 62. (MTRA 15:11)

1. Poltavskiy gosudarstvennyy pedagogicheskiy institut. (Naphthalenone) (Naphthenes)

KARISHIN, A. P.; KUSTOL, D. M.

Condensation of 5-iodoacenaphthenequinone with 3-hydroxythionaphthene and its derivatives. Zhur. ob. khim. 33 no.1: 203-204 '63. (MIRA 16:1)

1. Poltavskiy gosudarstvennyy pedagogicheskiy institut.

(Acenaphthenequinone) (Benzothiophene)

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